## MANUAL

## PHILIPS

## Cathode ray oscilloscope GM 5605

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## Important!

In correspondence concerning this apparatus please quote the type number and serial number as given on the plate at the back of the apparatus.

## GENERAL PART

## Introduction

The cathode ray oscilloscope GM 5605 has an extensive field of application and is particularly suitable for use in service workshops and for educational purposes. For X and Y deflection the apparatus contains d.c. amplifiers having the same properties (X-Y oscilloscope). The GM 5605 is, therefore, extremely suitable for displaying the relationship between two quantities, e.g. frequency and phase relationships. Moreover, voltages can be displayed as a function of time by means of the incorporated time-base generator.

## Technical data

Properties expressed in numerical values for which a tolerance has been stated are guaranteed at nominal mains voltages on the voltage adapter. Numerical values without tolerances indicate the properties of the average instrument and are only given for the information of the user.

Cathode-ray tube circuit
Tube
a. type
b. effective screen area
c. total accelerating voltage

Graticule

Y amplifier
Type
Deflection sensitivity

Frequency response
Overshoot
Sweep expansion

DH7-78 flat screen (other screen types can be supplied)
$6 \times 5 \mathrm{~cm}$ (width $\times$ height)
1750 V
$10 \times 8$ div. $(1 \mathrm{div} .=5.5 \mathrm{~mm})$
d.c. amplifier
adjustable to 8 calibrated values: 0.01-0.03-$0.1-0.3-1-3-10-30 \mathrm{~V} / \mathrm{div}$.
Tolerance: $\pm 3 \%$
Between the steps, the sensitivity can be continuously adjusted in a ratio of $1: 3.5$ (uncalibrated). $0-200 \mathrm{kc} / \mathrm{s}$ ( -3 dB ). Via the capacitor input the bandwidth is: $5 \mathrm{c} / \mathrm{s}-200 \mathrm{kc} / \mathrm{s}$.
$1 \%$ for pulses with a rise time of $\geqslant 25 \mathrm{~ns}$
$3 \times$ the useful screen height, i.e. $1.5 \times$ upwards and downwards from the centre.
At maximum expansion the peaks of the signal can be displayed undistorted by means of the vertical shift control.
Input
a. input sockets
b. input resistance
c. input capacitance
d. maximum permissible input voltage at d.c. input

4-mm plug sockets
$500 \mathrm{k} \Omega$
45 pF in position " $0.01 \mathrm{~V} /$ div." of the attenuator switch
25 pF in the positions " 0.03 " and " $0.1 \mathrm{~V} /$ div." 55 pF in the other positions.
400 Vr.m.s. $^{\text {. }}$

300 V

50 ms
e. Maximum permissible d.c. voltage at the a.c. input
f. RC time of the capacitor input

## X amplifier

Type
Deflection sensitivity

Response curve

Overshoot
Sweep expansion

Input
a. input sockets
b. input resistance
c. input capacitance
d. maximum permissible input voltage on d.c. input
e. Maximum permissible
d.c. voltage on the a.c. input
f. RC time of the capacitor input

Phase difference of the amplifiers

Phase difference

## Time base generator

Sweep times
Mode of operation
d.c. amplifier
adjustable to 7 calibrated values: 0.03-0.1-0.3-1-3-10-30 V/div. Tolerance: $\pm 3 \%$ Between the steps, the sensitivity can be continuously adjusted in a ratio of $1: 3.5$ (uncalibrated). $0-200 \mathrm{kc} / \mathrm{s}(-3 \mathrm{~dB})$. Via the capacitor input the bandwidth is: $5 \mathrm{c} / \mathrm{s}-200 \mathrm{kc} / \mathrm{s}$.
$1 \%$ for pulses with a rise time $\geqslant 25 \mathrm{~ns}$.
$3 \times$ the useful screen width, i.e. $1.5 \times$ to the left and to the right from the centre.
At maximum expansion the peaks of the signal can be displayed undistorted by means of the horizontal shift control.

4-mm plug sockets
$500 \mathrm{k} \Omega$
45 pF in position " $0.03 \mathrm{~V} / \mathrm{div}$ " of the attenuator switch
25 pF in the position " $0.1 \mathrm{~V} /$ div."
55 pF in the other positions.
$400 \mathrm{~V}_{\mathrm{r} . \mathrm{m} . \mathrm{s} .}$

300 V

50 ms
$\leqslant 5^{\circ}$ for frequencies of $0-200 \mathrm{kc} / \mathrm{s}$, provided that the two continuous attenuator controls are adjusted to " $\times 1$ ".
adjustable in 12 steps from $20 \mu \mathrm{~s} /$ div. to 100 $\mathrm{ms} / \mathrm{div}$. at a time base length of 10 divisions. triggered

## Triggering

a. required picture height for internal triggering
b. required voltage for external triggering
c. input impedance of socket "EXT.TRIGG."

## Supply

Mains voltage
internal or external
0.5 division for frequencies of $5 \mathrm{c} / \mathrm{s}-200 \mathrm{kc} / \mathrm{s}$.
$0.5 \mathrm{~V}_{\mathrm{p}-\mathrm{p}}$ for frequencies of $5 \mathrm{c} / \mathrm{s}-200 \mathrm{kc} / \mathrm{s}$.
The maximum voltage amounts to $10 \mathrm{~V}_{\mathrm{p}-\mathrm{p}}$ (in view of crosstalk).
$1 \mathrm{M} \Omega / / 20 \mathrm{pF}$
voltage adapter for $110-125-145-200-220$ and 245 V . The mains frequency may range from $40-100 \mathrm{c} / \mathrm{s}$ (mains frequencies $<50 \mathrm{c} / \mathrm{s}$ only at nominal mains voltage). Power consumption is 80 W .
The $Y$ and $X$ deflection sensitivity changes inversely proportional to the mains voltage.
height 25 cm
width 16 cm
depth 35 cm
10 kg

1 mains flex
1 manual
2 test cables

## DIRECTIONS FOR USE AND APPLICATIONS

## Installation

## A. ADJUSTING TO THE LOCAL MAINS VOLTAGE

The apparatus can be adjusted to mains voltages of 110-125-145-200-220 and 245 V by means of a voltage adapter.
The adjusted value can be read through the round opening in the rear panel. The instrument is adjusted to another mains voltage as follows.

- Remove the cover plate at the rear (Fig. 1).
- Pull the adapter out a little, turn it until the correct voltage value is uppermost and then press the adapter back again.
-- Refit the cover plate.



## B. EARTHING

Earth the instrument in accordance with the local safety regulations. This may be done

- via the mains flex, if the apparatus has a 3-core mains flex provided with a plug with rim-earthing contacts, or
- via one of the earthing sockets (" $\because$ ") at the front of the apparatus.

Double earthing connections may cause hum and must be avoided.

## C. CHECKING BEFORE SWITCHING ON

- Check the setting of the mains voltage adapter (see section A).
- Check whether the apparatus has been properly earthed (see section B).
- Set knob "INTENS." to position " 0 ".
- Connect the apparatus to the mains via the mains flex.


Fig. 2. If desired the apparatus can be tilted by means of the stand provided on the bottom

## D. SWITCHING ON

Switch on the apparatus by setting knob "INTENS." from position " 0 " to approximately its central position.

A stationary picture of maximum brightness, left on the screen for too long a time may permanently damage the screen.

## A. PRELIMINARY SETTING

- Set all knobs to the positions indicated in Fig. 3.
- Adjust the time base line to the centre of the screen by means ol the knobs " $\downarrow \mathrm{Y} \uparrow$ " and " $<-\mathrm{X} \rightarrow$ ".
- Check whether the time base line appears horizontally on the screen. If necessary, reposition the picture tube in accordance with section VI.H.1.
- Adjust the definition and the brightness of the picture by means of the controls "FOCUS." and "INTENS.".


Fig. 3. Preliminary setting

## Notes

- If the time base line cannot be displayed by means of knobs " $\leftarrow \mathbf{X} \rightarrow$ " and " $\uparrow \mathrm{Y} \downarrow$ ", potentiometer "DC-Balance" of the Y amplifier (accessible on the left-hand side of the apparatus) must be turned until the time base line appears. This potentiometer must be adjusted in such a way, that the picture does not shift if the continuous control "Y AMPL." is turned (see section V.F.1).
- If knob "X AMPL." is in position "0.3 V/div.", knob "DC-Balance" of the $X$ amplifier (accessible on the right-hand side of the apparatus) must be adjusted in such a way, that the light spot on the screen no longer shifts if the continuous control is turned (see section V.G. 1). With cathode ray tubes, astigmatism may arise. Then the light spot on the screen is not round. This can be corrected by means of potentiometer "ASTIGM.", accessible on the left-hand side of the apparatus.


## B. DISPLAYING WAVEFORMS

## 1. Time base internally triggered

- Adjust as described under "Preliminary setting" (page 14).
- Turn knob "STAB." anti-clockwise, until the time base line just disappears.
- Apply a voltage to the d.c. or a.c. input of the Y amplifier.
- Turn knob "STAB." until a stable picture is obtained.
- Place knobs "Y AMPL." and " $N$." in the required position.

Note: If no triggering occurs at minimum setting ( 0.5 div .), potentiometer "LEVEL" (R513, in the right-hand side wall) must be adjusted according to section V.H.I.

## 2. Time base externally triggered

- Adjust as described under "Preliminary setting" (page 14).
- Turn knob "STAB." anti-clockwise until the time base line just disappears.
- Apply a voltage to the d.c. or a.c. input of the Y amplifier.
- Apply an external trigger voltage to socket "EXT.TRIGG." on the right-hand side of the apparatus (if the picture must be stationary, this voltage must be derived from the voltage from which the $Y$ signal also originates).
- Place knobs "Y AMPL." and " $M$ " at the required position.


## C. HOW TO USE THE X INPUT

If a voltage is applied to both amplifiers, these voltages can be compared with each other and their relationships can be made visible.
Some of these applications are also mentioned in chapter III.

- Connect the voltages to be compared to the input sockets "DC (AC) Y AMPL." and "DC (AC) X AMPL.".
- Place switches "Y AMPL." and "X AMPL." in the desired position.
- Set the continuous control "X AMPL" to position " $\times I$ ".

The picture can now be brought on the screen by means of the shift controls " $\downarrow \mathrm{Y} \uparrow$ " and " $<\mathrm{X} \rightarrow$ ".
In order to obtain good stationary pictures, the voltages on the two amplifier inputs should be synchronous.


Fig. 4. Functions of the controls and sockets

## Applications

## A. MEASURING THE AMPLITUDE

- Measure the distance between the peaks, c.g. 3 div. (see Fig. 5).
- Determine the position of knob "Y AMPI.." (continuous attenuator in position " $\times 1$ "), c.g. $10 \mathrm{~V} /$ div.
Now the amplitude amounts to 10 (attenuator position) $\times 3$ (picture height) $=30 \mathrm{~V}$.


Fig. 5. Measuring the amplitude

## B. USING THE X INPUT

The following examples can be mentioned:
Frequency measurements
Phase measurements
Displaying characteristics
Etc.
Frequency measurement by means of Lissajous figures
If a voltage of unknown frequency is applied 10 the $Y$ amplifier, the light spot on the screen will describe a so-called Lissajous figure, under the influence of a voltage of known frequency applied to the X amplifier. Dependent on the frequency the image will show a certain number of peaks. The unknown frequency
$\mathrm{f}_{\mathrm{x}}=\frac{\text { number of peaks at the top }}{\text { number of peaks at the side }} \times$ known frequency.
Some common Lissajous figures are shown in Fig. 6, in which $50 \mathrm{c} / \mathrm{s}$ is used as reference frequency.


Fig. 6. Examples of Lissajous figures

## Phase measurements

Phase angles can be measured by means of a Lissajous figure (ellipse)
The image must then lie symmetrically round the centre.
The following applies irrespective of the quadrant in which the phase angle is found: the sine of phase angle $\varphi$ is determined by the ratio $a / b$ (see Fig. 7).
In the figure, sine $\varphi=2 \mathrm{div} . / 4 \mathrm{div} .=0.5$. The phase angle $\varphi$ is then $30^{\circ}$. If the top of the ellipse is at the right of the screen, the phase angle is in the first quadrant $\left(30^{\circ}\right)$ or in the fourth quadrant $\left(360^{\circ}-30^{\circ}=330^{\circ}\right)$.


Fig. 7. Determining the phase angles sine $\varphi=a / b$

If the top is at the left of the screen, the angle is in the second quadrant $\left(180^{\circ}-30^{\circ}=150^{\circ}\right)$ or in the third quadrant $\left(180+30^{\circ}=210^{\circ}\right)$. For determination of the quadrant proceed as follows:

- Include a circuit as shown in Fig. 8 into the lead to the X amplifier with closed switch.
- Open the switch and turn the potentiometer from minimum to maximum value. In doing so, the shape of the ellipse must clearly change.


Fig. 8. Network for quadrant determination

Phase angle (thus also a) Quadrant Quadrant
becomes

| larger | 2. $\left(90^{\circ}-180^{\circ}\right)$ | 1. $\left(0^{\circ}-90^{\circ}\right)$ |
| :--- | :--- | :--- |
| smaller | 3. $\left(180^{\circ}-270^{\circ}\right)$ | 4. $\left(270^{\circ}-360^{\circ}\right)$ |

If the picture appears as a straight diagonal on the screen, the phase angle is $0^{\circ}\left(360^{\circ}\right)$ or $180^{\circ}$ (Fig. 9).


Fig. 9. Some particular phase angles

## C. DISPLAYING A DIODE CHARACTERISTIC

In displaying a diode characteristic the current through the diode is plotted as a function of the voltage across the diode. For this, use can be made of the circuit shown in Fig. 10. Voltage source E supplies a low sinewave voltage. The resistance R must be small with respect to the expected internal resistance of the diode. The voltage across $R$, which is directly proportional to the anode current, is fed to the $Y$ amplifier. The anode voltage is applied to the X amplifier. Now a curve is displayed which represents the relationship between anode current and anode voltage.


Fig. 10. Displaying the diode characteristic of the OA 85

## D. DISPLAYING A HYSTERESIS LOOP

In displaying hysteresis loops of magnetic material, the magnetic induction B is plotted as a function of the field strength H . If the iron core of a coil contains no air gaps, the field strength is proportional to the current through the number of windings. The primary current is thus a measure of the field strength H . A resistor Rp is connected in series with the primary winding. The voltage across this resistor is applied to the X input (see Fig. 12).
The voltage across the secondary winding is $U s=k \cdot d B / d t$.
Here k is a constant.
This voltage is integrated by an RC network ( $R \gg 1 / \omega \mathrm{c}$ ). The voltage across the capacitor then becomes $U c=k \cdot B / R . C$. The induction $B$ is thus proportional to the voltage across the capacitor. This voltage, which is low and must be adequately amplified, is fed to the Y amplifier.



Fig. 11. Displaying a hysteresis loop

Note - It is possible that the trace is displayed as a mirror image with respect to the $Y$ axis. The peak of the hysteresis loop is brought to the right of the sercen by reversing the connections of one of the coil windings.

## SERVICE DATA

## Circuit diagram

## A. Y AMPLIFIER (unit A, Fig. 29)

The amplifier for the Y deflection is a d.c. coupled push-pull amplifier. The voltage under test is connected to socket BU2 (DC) or to socket BU3 (AC) and subsequently applied to the output amplifier via an attenuator circuit and a phase inverter.

## 1. Attenuator circuit

An attenuator circuit, which is operated by means of SK3, is included in the input circuit of the Y amplifier.
In the positions " $3 \mathrm{~V} / \mathrm{div}$." and " $10 \mathrm{~V} / \mathrm{div}$." ofSK3, the signal to be measured is attenuated by the voltage dividers R34-R26//R41 and R35-R27//R41 A step attenuator with high impedance (R36-R28 ... R32) is included in the other positions of SK3. The attenuator switch has eight calibrated positions. By means of the trimmers C27, C28 and C29 and the capacitors C30, C31, C32 and C33, the attenuators are adjusted in such a way that in all positions of SK3 the attenuation is frequency independent.

## 2. Phase inverter stage

Via the attenuator circuit the signal to be measured is applied to the phase inverter stage with the valves B1 and B2. This stage is driven on the control grid of valve B1. Valves B1 and B2 are coupled via the common cathode resistor R40. As the control grid of B 2 is connected to earth via R42, this valve is driven by a voltage whose magnitude is equal to the signal to be measured, but opposed in phase to the latter. The voltage on the anodes of B1 and B2 are symmetrical with respect to the average d.c. voltage difference between these anodes.
The amplitude of the signal can be adjusted continuously by varying the value of the anode resistors R43 and R49 - and thus the amplification by means of potentiometer R6.
Turning potentiometer R6 would also result in a variation of the average d.c. voltage on the input of the next amplifier stage ( $\mathrm{BI}^{\prime}-\mathrm{B} 2^{\prime}$ ), which would
give rise to a shift of the light spot on the screen. This is avoided by equalizing the values of the d.c. voltages on the anodes of $\mathrm{Bl}^{\prime}$ and B 2 ' by means of potentiometer R57 (DC-Balance), so that no d.c. voltage arises across R6.
Resistor R37 in the control grid circuit of valve B1 serves to limit the grid current in the case of positive input signals. The adverse influence of this resistor on the square wave response is eliminated by parallel capacitor C34.

## 3. Output stage

Output amplifier $\mathrm{B} 3-\mathrm{B} 3^{\prime}$ is preceded by the cathode followers $\mathrm{B} 1^{\prime}$ and B2', which are provided to reduce the influence of the high input capacitance of the output valves on the anode impedance of the valves Bl and B 2 . As a result the bandwidth of the amplifier is larger than if the valves B 1 and B 3 or B 2 and $\mathrm{B} 3^{\prime}$ were directly coupled to the preceding stage. The shift controls R4-R4' are included in the control grid circuit of the cathode followers. By means of these potentiometers the d.c. voltage on the control grids of $\mathrm{B} 1^{\prime}$ and $\mathrm{B} 2^{\prime}$ can be varied. The variation on the grid of $\mathrm{Bl}^{\prime}$ opposite to that on the grid of $\mathrm{B}^{\prime}$. As a result the image will shift in the vertical direction across the screen. The shift voltage is applied to the control grids of $\mathrm{B} 1^{\prime}$ and $\mathrm{B} 2^{\prime}$ via the voltage dividers with high impedance $\mathrm{R} 76-\mathrm{R} 64$ and $\mathrm{R} 72-\mathrm{R} 70$ respectively. By means of these voltage dividers the anode potentials of valves $B 1$ and $B 2$ are made independent of the position of the shift controls (R4, R4'), so that the d.c. balance is maintained. Capacitors C36 and C37 prevent the voltage dividers from affecting the square wave response. By means of potentiometer R80 the feedback of both output valves is adjusted in such a way that the maximum $Y$ sensitivity is $10 \mathrm{mV} \mathrm{V}_{\mathrm{p}-\mathrm{p}} / \mathrm{div}$.
The symmetry of the signal in the output stage is increased due to the common cathode resistor. The anodes of B3 and B3' are directly connected to the Y deflection plates. For driving the time base generator in the case of internal triggering use is made of that part of the anode voltage of B3, which is applied to the first valve (B501) of the trigger pulse shaper via switch SK5.

## B. TRIGGER PULSE SHAPER (unit D, Fig. 31)

The trigger pulse shaper consists of an amplifier stage (B501) and a Schmitt trigger (B502-B502').
The trigger signal, which may originate from the $Y$ amplifier (R85) as well as from an external voltage source, is applied to the control grid of
valve B501 via C501. The anode of this amplifier valve is d.c. coupled to the input of the Schmitt trigger (B502-B502'). A Schmitt trigger is a multivibrator with two stable conditions, viz.
B502 conductive, B502' cut off, and
B502 cut off, B502' conductive.
The condition is changed by applying a positive pulse to the control grid of the non-conductive valve or a negative pulse to the grid of the conductive valve. By means of R513 the Schmitt trigger B502-B502' is adjusted in such a way that in the waiting position (i.e. if no trigger voltage is applied) valve B502 is cut off and B502' conductive. During the positivegoing part of the cycle the amplified trigger signal applied to the control grid of B502 will drive the valve into conduction at a certain level (the upper threshold voltage). Due to the common cathode resistor and the d.c. coupling between the anode of valve B502 and the control grid of valve B502' a cumulative switching phenomenon takes place, as a result of which valve B502' is cut-off. This results in a positive voltage at the anode of B502'.

During the negative half of the cycle of the amplified trigger signal, valve B502 will be cut-off at a certain level (lower "threshold voltage"). Due to the repetitive switching action, valve B502' becomes conductive, so that a negative voltage arises at the anode of this valve. In the case of a repetitive trigger signal it is necessary for the correct functioning of the trigger pulse shaper that both threshold voltages are exceeded. The trigger sensitivity of the trigger pulse shaper is thus determined by the difference in level between the two threshold voltages. This difference is adjusted by means of potentiometer R513, so that the position of this potentiometer is decisive for the trigger sensitivity.
The positive and negative voltage transients at the anode of valve B502' are differentiated by capacitor C503 and resistor R521 into small positive and negative pulses, which are applied to the Schmitt trigger B503B503' in the time base generator.
The control range of R 3 is adjusted by selection of resistor R 522 . The capacitors C502 and C517 in the anode leads of valves B502 and B501 respectively serve to improve the rise time of the pulse shaped voltages.

## C. TIME BASE GENERATOR (unit D, Fig. 31)

## 1. Principle

The sawtooth voltage is obtained by means of a Schmitt trigger and a "bootstrap" integrator. The working of the Schmitt trigger is the same as that of the trigger described in chapter B "Trigger pulse shaper". By means of potentiometer R3 ("STAB.") the multivibrator is adjusted in such a way that it can operate both free running and triggered. R3, however, must be so adjusted that valve B503' is cut-off and B503 conductive (in that case no time-base line is visible on the screen). In this condition, the control grid potential of B503 is equal to the cathode potential of this valve, because the control grid is connected to the positive supply voltage via R530-R531 and GR503. The working principle of the "bootstrap" integrator is shown in the figure below.


This circuit ensures that the charging current of capacitor $C$ remains constant, independent of the charge of capacitor $C$, so that the charge curve is of good linearity.
A voltage variation across capacitor $C$ is applied to resistor $R$ via an amplifier with an amplification factor $A \approx 1$ and battery $E$.
The voltage across resistor R - and thus the charging current through the capacitor -- therefore remains constant, which results in a linear charge curve of the capacitor.

## 2. Working

The circuit employed in the GM 5605 is shown in Fig. 13.
If no trigger signal is applied, the potential on the control grid of valve B501' is determined by the cathode voltage of valve B503. The voltage across the time base capacitor (C505... C516) is then almost equal to this cathode voltage, which amounts to approximately 100 V .
As soon as a trigger voltage is applied, valve B503 is made non-conductive by the positive trigger pulses at the cathode of B503. Owing to the repetitive switching action, the condition of the multivibrator changes into B503' conductive and B503 cut-off. Now the potential of the control grid of B501' is undefinite, but in principle will tend to rise to the anode potential of valve B501'. However, the time base capacitor does not allow a sudden voltage rise, but will be charged in accordance with an e-power curve. Owing to the charging, the control grid potential of valse


B501' will rise a little, as a result of which the cathode potential rises to the same extent. This voltage rise is applied to the cathode of diode GR503 via capacitor C518, so that the diode is cut-off. The voltage across resistor R531 + R533 thus remains constant.
If the voltage across the time base capacitor rises further, the process described will be continued. The time base capacitor is thus charged by
a constant current supplied by capacitor C518, as a result of which the voltage across this capacitor increases linearly (this is the forward sweep of the sawtooth voltage). As soon as the amplitude of the sawtooth voltage has reached a given value, valve B503 becomes conductive. As a result the Schmitt trigger B503-B503' switches over to the condition B503 conductive - B503' cut-off. The voltage on the control grid of B503 then drops to the cathode voltage of valve B503. The resultant grid current of valve B503 causes the control grid voltage of valve B501' to drop likewise. This voltage drop is applied to the cathode of diode GR503 via valve B501' connected as a cathode follower and capacitor C518. This diode becomes again conductive and the potential of the junction R531-C518 is again determined exclusively by the potential of the anode of valve $\mathrm{B} 501^{\prime}$. In this period the time base capacitor discharges across R530, across the diode formed by the control grid and the cathode of valve B503 and across resistor R521 until the voltage across the capacitor is equal to the cathode voltage of B503 (this is the flyback of the sawtooth voltage). At the end of the flyback C518 is charged again via diode GR503 and the low output impedance of cathode follower B501'. This condition, the waiting period, is maintained until multivibrator B503B503' is again changed over by a trigger pulse.

## 3. Linearity of the sawtooth voltage

The sawtooth voltage has a good linearity due to the good transmission of the cathode follower, the large capacitance of capacitor C518 and the use of diode GR503.

## 4. Sweep time

The slope of the sawtooth voltage - and thus the sweep time per divisiondepends upon both the value of the time base capacitor and the charging current. The sweep time can thus be varied by changing the value of the time base capacitor. The time base capacitors are selected with SK2, by means of which twelve sweep times can be adjusted. By means of R533 the charging current is adjusted in such a way that the sweep times per unit of length comply with the orientation values on the text plate to within $25 \%$.

## 5. Sawtooth voltage

The sawtooth voltage is available across resistor R733 (Fig. 33). The amplitude of the voltage applied to the X amplifier is determined by the value of R733.
D. X AMPLIFIER (unit C, Fig. 33)

Except for the input circuit and the anode circuit of valve B703 the X amplifier is equal to the Y amplifier.

## 1. Input circuit

As desired, either an external voltage or the sawtooth voltage can be applied to the X amplifier. In the first position of SK4 the sawtooth voltage is taken from resistor R733 and applied to the input of the amplifier. An external deflection voltage can be applied directly (via socket BU4) or via an isolating capacitor (via socket BUS).
The position of the time base line on the screen is determined by the potential on the control grid of valve B702. This potential can be adjusted by means of potentiometer R746. In the other positions of SK4 the control grid is connected to earth via R746 and at the same time the screen grid voltages of the valves B501 and B503 are switched off. As a result the time base generator no longer starts, so that there is no risk of crosstalk in the $X$ amplifier.
The attenuator circuit, which is operated with switch SK4, is built up in the same way as the circuit of the Y amplifier. The only difference is that the step attenuator has only four possibilities of attenuation, so that the deflection sensitivity of the X amplifier can be adjusted to seven values. By means of trimmers C727, C728 and C729 and capacitors C733, C730, C731 and C732 the attenuators are adjusted in such a way that in all positions of SK4 the attenuation is frequency independent.

## 2. Amplifier stages

The amplifier stages are practically identical to those of the Y amplifier. The difference is that the anode resistor of B703 is not divided into two halves, as the anode resistor of B3. The anode potentials of valves B701 and B702 are equalized by means of R757 (DC-Balance), so that the image does not shift in the horizontal direction if continuous attenuator R7 is turned. With the double potentiometer R5-R5' the image can be shifted horizontally across the screen. By means of R780 the sensitivity of the amplifier is adjusted to $30 \mathrm{mV} \mathrm{V}_{\mathrm{p}-\mathrm{p}} /$ div.
The anodes of the valves B703 and B703' are directly coupled to the X deflection plates.

## E. CATHODE RAY TUBE CIRCUIT (unit B, Fig. 35)

1. Intensity and brightness control

The brightness of the picture can be changed by varying the potential on the Wehnelt cyclinder by means of R1.
A pulse-shaped voltage, which is applied to the Wehnelt cylinder via capacitor C519, is taken from the anode of B503. This pulse-shaped voltage is high during the forward sweep of the sawtooth voltage and low during the flyback. As a result the electron beam is suppressed during the flyback of the sawtooth voltage, because the positive peak of the pulseshaped voltage is retained by diode GR301 almost on the level adjusted with R1. Capacitor C301 serves to prevent crosstalk of the brightness pulse on the negative supply voltage and to smooth the ripple of the negative supply part.

## 2. Focusing and astigmatism

The line on the screen can be adjusted sharply by means of potentiometer R2. This potentiometer regulates the voltage on the focusing anode g3 of valve B301. Astigmatism of the electrostatic lens can be corrected by adjusting the voltage on the last acceleration anode (g4) to the correct value by means of potentiometer R305.

## 3. Barrel and pincushion distortion

This is due to faults (for instance fringe areas) in the electrostatic lens and can be corrected by adjusting the voltage at the beginning of the postaccelerating coil to a certain value by means of potentiometer R309.

## F. SUPPLY PART (unit E, F, Fig. 38)

The supply part delivers voltages of $+280 \mathrm{~V},+160 \mathrm{~V},-150 \mathrm{~V}$ and +1610 V .
The voltage of +280 V is electronically regulated and stabilised.

1. +280 V

The Graetz circuit GR 1001 . . GR 1004 supplies a full-wave rectified voltage, which is applied to the control circuit.
This control circuit consists of a series regulator (B 1001), control valve (B1001') and a stabiliser (B1002). The latter keeps the cathode of B1001' at a constant potential of 85 V . A load variation or mains voltage variation in the $+280-\mathrm{V}$ supply circuit will result in a change of the $+280-\mathrm{V}$
voltage. This voltage variation is passed to the control grid of valve B1001 via the voltage divider R1009//R1012-R1011. The voltage applied to the control grid is considerably amplified owing to the large anode resistor (R1005).
From the anode of valve BI001' the amplified signal, which is opposed in phase to the original voltage variation, is applied to the control grid of series regulator B1001. As a result this valve, dependent upon a positive or negative voltage variation of the $+280-\mathrm{V}$ voltage, will carry less or more current, so that the original voltage variation is compensated for. The ripple voltage on the $+280-\mathrm{V}$ voltage is also fed back. The feedback factor for the ripple voltage is, however, much greater than that for the d.c. voltage, due to the use of capacitor C1003 in parallel with R1009.

The current which must be supplied by the $+280-\mathrm{V}$ supply part is larger than that supplied by the series regulator. Resistor R1003 is, therefore, connected in parallel with B1001.
Voltage divider R1003-R1004 is provided for hum compensation.
2. +160 V

This voltage is derived from the $+280-\mathrm{V}$ supply voltage by means of voltage divider R1019-R1020.
3. -150 V

This is the full-wave rectified and smoothed a.c. voltage supplied by winding S3 of the supply transformer.
The voltage of -150 V is among others applied to the Wehnelt cylinder of the cathode ray tube via R1.
The brightness of the picture can thus be adjusted by means of potentiometer R1.
4. +1610 V

The a.c. voltage taken from winding S7 of the supply transformer is halfwave rectified by means of valve B1003. The rectified voltage is applied to the post-acceleration anode of the cathode ray tube.

## 5. Heater voltage

The heater voltages for the various valves are derived from windings S 4 , S5, S6 and S8.
The windings S 5 and S 6 are brought at a d.c. voltage potential.
This prevents breakdown in case the maximum permissible voltage difference between heater and cathode is exceeded.

## Gaining acces to the parts

## A. REMOVING THE CABINET PANELS

The cabinet consists of a number of separate panels, which may be removed individually.

## Rear panel

This may be removed after the two screws " $A$ " on the rear panel have been loosened a few turns (Fig. 14).

## Top panel

After the rear panel has been detached, the top panel may be removed by loosening the two screws "B" a few turns (Fig. 14).


Fig. 14. Removing the cabinet panels

## Side panels

After the rear panel has been detached, the side panels may be removed by sliding them slightly backwards and subsequently lifting them sideways out of the frame.

## Bottom panel

After detaching the rear panel, the bottom panel may be removed by unscrewing the four screws "C" (Fig. 16).

## B. REMOVING THE KNOBS (Fig. 15)

## Single knobs

- Remove cap "A".
- Loosen nut "B". The knob may now be slid off the spindle.


## Double knobs

- Remove cap "A".
- Loosen nut "B". Now the smallest knob can be slid off the spindle.
- Loosen nut "C". Now the large knob can be slid off the spindle.


Fig. 15. Removing the knobs

## C. REMOVING THE FRONT PANEL

- Remove the cabinet panels according to section II.A.
- Remove the knobs according to section II.B.
- Unsolder the connecting wires of sockets BUl and BU6.
- Unscrew the rings of sockets BU2 . . BU5.
- Remove the 10 screws "S" (Fig. 16).
- Remove the front panel (consisting of front frame and text plate).


Fig. 16. Removing the bottom plate and front panel

## D. REMOVING THE WINDOW AND THE GRATICULE

- Turn the window approximately $15^{\circ}$ anticlockwise and remove it from the front panel (Fig. 17).
Now the graticule can be pushed out of the window.
- The window can be adjusted horizontally by moving the stop bracket at the rear of the front panel. Before moving the bracket, first loosen the two fixing screws a little.


## GM 5605 nervily <br> Gaining access to the parts



Fig. 17. Removing the graticule

## Maintenance

A. WAFER SWITCHES

If these switches no longer function properly due to soiling, they can be lubricated with switch oil (see "List of mechanical parts", page 56). This oil has both cleaning and lubricating properties. After lubrication, the switch must be rotated a few times through all positions.

## B. CABINET PANELS

If the PVC-coated cabinet panels have become dirty they can, after removal, be washed with water and soap (Chapter II.A); if necessary, use some scouring powder.

## Adjusting elements and their functions

The sequence below is arbitrary. For complete adjustment it is advisable to adhere to the sequence given in Chapter V.

| Adjustment | Adjusting <br> element | Measuring instrument | Recommen PHILIPS apparatus | Chapt. section |
| :---: | :---: | :---: | :---: | :---: |
| Barrel or pincushion distortion | R309 | L.F. generator | GM 2317 | D |
| Astigmatism | R305 | L.F. generator | GM 2317 | E |
| Control range R2 | R304 | L.F. generator | GM 2317 | E |
| Y amplifier |  |  |  |  |
| - Zero setting | R57 | None |  | F1 |
| - Sensitivity | R80 | L.F. generator | GM 2317 | F2 |
| - Square wave response SK3 | $\begin{aligned} & \mathrm{C} 27, \mathrm{C} 28, \\ & \mathrm{C} 29 \end{aligned}$ | Square wave voltage generator | GM 2324 | F4 |
| X amplifier |  |  |  |  |
| - Zero setting | R757 | None |  | G1 |
| - Sensitivity | R780 | L.F. generator | GM 2317 | G2 |
| - Length of time base line | $\begin{aligned} & \text { R733, } \\ & \text { R746 } \end{aligned}$ | None |  | G3 |
| - Square wave response SK4 | $\begin{aligned} & \mathrm{C} 727, \\ & \mathrm{C} 728, \\ & \mathrm{C} 729 \end{aligned}$ | Square wave voltage generator | GM 2324 | G5 |
| - Phase characteristic | C39 | L.F. generator | ZV 2312 | G10 |
| Time base generator |  |  |  |  |
| -- Internal triggering | R513 | L.F. generator | ZV 2312 | H1 |
| - Stability | R522 |  |  | G3 |
| - Sweep times | R533 |  |  | H4 |

## Supply

| - Ripple voltage on <br> $+280 ~ V$ | R1004 | L.F. a.c. voltmeter | GM 6012 | C |
| :--- | :--- | :--- | :--- | :--- |
| $-+280-$ V voltage | R1011 | d.c. voltmeter | GM 6058 | B |

## Checking and adjusting

The tolerances given below are factory tolerances, which apply only if the apparatus is readjusted. They may deviate from the tolerances mentioned in the technical data (General part, chapter II).

A survey of the adjusting elements and their functions is given on page 37.

## A. MAINS CURRENT

At $220 \mathrm{~V}, 50 \mathrm{c} / \mathrm{s}$ the current taken from the mains must not exceed 420 mA .

## B. SUPPLY VOLTAGE +280 V

Check whether the supply voltage on the cathode of valve B1001 is between 278 V and 282 V . If necessary, select another value for R1011.

## C. RIPPLE ON THE SUPPLY VOLTAGE +280 V

Check whether the ripple voltage on the cathode of valve B1001 does not excced 10 mV . If necessary, select another value for R1004.

## D. BARREL AND PINCUSHION DISTORTION

- Apply a sinusoidal voltage of $50 \mathrm{c} / \mathrm{s}$ to BU3.
- Also apply a sinusoidal voltage to BU5, however, of a frequency of $10 \mathrm{kc} / \mathrm{s}$.
- Adjust the amplitudes of both voltages in such a way that a uniformly lit square of $7.5 \times 7.5$ divisions is obtained.
- Reduce a possible barrel or pincushion distortion to minimum by means of R309. When adjusted correctly, no point of the sides of the square must fall within a concentric square of $7 \times 7$ divisions.
-- Display a line on the screen which makes an angle of $30^{\circ}$ with the Y axis. (Two voltages of equal phase, frequency $1 \mathrm{kc} / \mathrm{s}$, on BU3 and BU5).
- Check that this line is straight.

If necessary, adjust R309 in such a way that both requirements are met as far as possible.

## E. FOCUSING AND ASTIGMATISM

- Display a circle of a diameter of 4 cm on the screen (apply (wn simusoidal voltages with a phase difference of $90^{\circ}$ to the $X$ and $Y$ infull).
- Set R305 in such a way that the picture can be adjusiced sharply by means of R2, both at high and low brightness.
- If necessary, select another value for R304.


## F. Y AMPLIFIER

## 1. Zero setting

- Set SK3 to position "30 V/div.".
- Set SK4 to position " $N$.".
- Turn R3 clockwise.
- Adjust the time base line to the centre of the scrien by mbillis of R4.
- Adjust R57 in such a way that the line does not move. il R6, is lurned (with shorted input).


## 2. Sensitivity

- Set SK3 to position ". $01 \mathrm{~V} / \mathrm{div}$.".
- Turn R6 clockwise, R7 anti-clockwise and R513 clockwise.
- Set SK8 to position " $M$ '.
- Adjust R3 in such a way that the time base generator just culs curt.
- Apply to BU2, a voltage of $80 \mathrm{mV}_{\mathrm{p}-\mathrm{p}}$, frequency $2 \mathrm{kc} / \mathrm{s}$.
- Adjust R513 in such a way that a triggered image appears.
- Adjust R80 in such a way that the picture height is 8 divisions.


## 3. Y shift

- Apply a sinusoidal voltage (frequency $2 \mathrm{kc} / \mathrm{s}$ ) to BU2 of such a value that the picture height is 3 divisions (the voltage must be symmetrical with respect to earth).
- Increase the input voltage by a factor 8.
- Both with R4 fully anti-clockwise and fully clockwise it must be possible to display the peaks of the sinewaves undistorted within the praticule. If necessary, replace valves B1 and B2 and repeat the adjustiment from item Fl onwards.


## 4. Step attenuator

Check the attenuation with SK3 in the following positions (R6 fully clockwise):
$\left.\begin{array}{crr}\hline \text { Position SK3 } & \text { Voltage on BU2 } & \text { Picture height } \\ \hline .01 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 28.25 \mathrm{mV}_{\text {r.m.s. }} \\ .03 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 84.75 \mathrm{mV}_{\text {r.m.s. }} \\ .1 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 0.2825 & \mathrm{~V}_{\text {r.m.s. }} \\ .3 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 0.8475 & \mathrm{~V}_{\text {r.m.s. }} \\ 1 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 2.825 & \mathrm{~V}_{\text {r.m.s. }} \\ 3 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 8.475 & \mathrm{~V}_{\text {r.m.s. }} \\ 10 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 28.25 & \mathrm{~V}_{\text {r.m.s. }} \\ 30 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 84.75 & \mathrm{~V}_{\text {r.m.s. }}\end{array}\right\}$

## 5. Continuous attenuator

- Turn R6 fully clockwise.
- Apply a sinusoidal voltage to BU2 of a frequency of $2 \mathrm{kc} / \mathrm{s}$ and an amplitude such that the picture height amounts to 3.5 divisions.
- Turn R6 fully anti-clockwise.

The picture height must now lie between 0.7 and 1 division.

## 6. Square wave response

- Turn R6 clockwise.
- Set SK 3 to position ". $01 \mathrm{~V} /$ div."
- Apply a square wave voltage of a frequency of $2 \mathrm{kc} / \mathrm{s}$ to BU2. The picture height must amount to approximately 8 divisions.
- Compare the square wave response with Fig. 18.


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Fig. 18. Square wave response of the $Y$ amplifier

## 7. Square wave response of step attenuator

- Turn R6 fully clockwise.
- Connect a square wave voltage of a frequency of $2 \mathrm{kc} / \mathrm{s}$ to BU2.
- Adjust the square wave response according to the table below:

| Position SK3 | Adjust with |
| :--- | :--- |
| $.03 \mathrm{~V} / \mathrm{div}$ | C27 (see Fig. 18) |
| $.1 \mathrm{~V} / \mathrm{div}$ | C28 (see Fig. 18) |
| $.3 \mathrm{~V} / \mathrm{div}$ | C 29 (see Fig. 18) |

Check the other positions.

## 8. Amplitude/frequency characteristic

- Turn R6 fully clockwise.
- Set SK3 to position ". $01 \mathrm{~V} / \mathrm{div}^{\prime}$ ".
- To BU2 apply a sinewave voltage of a frequency of $2 \mathrm{kc} / \mathrm{s}$ and an amplitude such that the picture height is 8 divisions. If the sensitivity is adjusted correctly (see item 2), the voltage on BU2 must amount to approximately $28.3 \mathrm{mV}_{\text {r.m.s. }}$
- Increase the frequency of the voltage on BU2 to $200 \mathrm{kc} / \mathrm{s}$, but keep the amplitude constant. Now the picture height must be at least 6 divisions.
- Check whether a d.c. voltage connected to BU3 is blocked by the builtin isolating capacitor C26.


## 9. Hum in the $Y$ amplifier

The hum in the Y amplifier must not exceed 0.2 divisions with SK3 in position ". $01 \mathrm{~V} / \mathrm{div}$.".

## G. X AMPLIFIER

1. Zero setting

- Set SK4 to position " $30 \mathrm{~V} /$ div.".
- Adjust the spot to the centre of the screen by means of R5.
- Adjust R757 in such a way that the spot does not move if R7 is turned (with shorted input).


## 2. Sensitivity

- Set SK4 to position ". $03 \mathrm{~V} / \mathrm{div}$.".
- Turn R7 clockwise.
- To BU5 apply a signal of $300 \mathrm{mV}_{\mathrm{p}-\mathrm{p}}$ of a frequency of $1 \mathrm{kc} / \mathrm{s}$.
- Adjust R780 in such a way that the horizontal deflection covers 10 divisions.

3. Length of the time base line

- Set SK4 to position " $N$ ". No input voltage on the input sockets.
- Turn R7 fully anti-clockwise.
- By means of R5 adjust the spot to the centre of the screen.
- Set SK2 to position " $2 \mathrm{msec} / \mathrm{div}$ ".
- With R3 set at $45^{\circ}$ from the left-hand stop, adjust the time base generator to free-run by means of R522 (in doing so, the apparatus must be at operating temperature).
- Adjust R746 in such a way that the time base line is symmetrical with respect to the centre of the screen.
- Select such a value for R733 that the length of the time base line lies between 11 and 13 divisions in all positions of SK2.
- If necessary, readjust R746.


## 4. X shift

- Apply a sawtooth voltage to BU3.
- To BU5 apply a sinusoidal voltage of a frequency of $2 \mathrm{kc} / \mathrm{s}$ and an amplitude such that the picture height is 3 divisions (the voltage must be symmetrical with respect to earth).
- Increase the amplitude of the input signal by a factor 10 .
- Both with R5 fully anti-clockwise and fully clockwise it must be possible to display the peaks of the sinewaves undistorted within the graticule.

If necessary, valves B701 and B702 may be replaced and the adjustment repeated from item El onwards.

## 5. Step attenuator

Check the attenuation with SK4 in the following positions (R7 fully clockwise):
$\left.\begin{array}{lll}\hline \text { Position SK4 } & \text { Voltage on BU4 } & \text { Picture width } \\ \hline .03 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 84.75 \mathrm{mV}_{\text {r.m.s. }} \\ .1 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} \text { /div. } & 0.2825 \mathrm{~V}_{\text {r.m.s. }} \\ .3 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 0.8475 \mathrm{~V}_{\text {r.m.s. }} \\ 1 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 2.825 \mathrm{~V}_{\text {r.m.s. }} \\ 3 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 8.475 \mathrm{~V}_{\text {r.m.s. }} \\ 10 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 28.26 \mathrm{~V}_{\text {r.m.s. }} \\ 30 \mathrm{~V}_{\mathrm{p}-\mathrm{p}} / \text { div. } & 84.75 \mathrm{~V}_{\text {r.m.s. }}\end{array}\right\}$

## 6. Continuous attenuator

- Turn R7 fully clockwise.
- To BU4 apply a sinewave voltage of a frequency of $2 \mathrm{kc} / \mathrm{s}$ and an amplitude such that the picture height is 3.5 divisions.
- Turn R7 fully anti-clockwise.
- Now the picture width must be between 0.7 and 1 division.


## 7. Square wave response

- Turn SK4 and R7 fully clockwise.
- Apply a square wave voltage to BU4 of a frequency of $2 \mathrm{kc} / \mathrm{s}$. The picture width must be approximately 8 divisions.
- The square wave response must at least be in accordance with Fig. 19.


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Fig. 19. Square wave response of the $X$ amplifier

## 8. Square wave response of step attenuator

- Turn R7 fully clockwise.
- To BU4 connect a square wave voltage of a frequency of $2 \mathrm{kc} / \mathrm{s}$.
- Adjust the square wave response according to the table below.

Position SK4 Adjust with
$0.1 \mathrm{~V} /$ div. $\quad \mathrm{C} 727$ (Fig. 19)
0.3 V/div. C728 (Fig. 19)

1 V/div. C729 (Fig. 19)
Check the other positions.

## 9. Frequency response curve

- Turn SK4 and R7 fully clockwise.
- Set SK3 to position " $30 \mathrm{mV} /$ div.".
- To BU4 connect a sinewave of a frequency of $2 \mathrm{kc} / \mathrm{s}$ and an amplitude such that the picture width is exactly 8 divisions. If the $X$ sensitivity (see point E.2) is correctly adjusted, the voltage on BU4 must amount to about 85 mV .
- Increase the frequency of the voltage on BU4 to $200 \mathrm{kc} / \mathrm{s}$, but keep the amplitude constant. Now the picture width must be at least 6 divisions.


## 10. Phase characteristic

- Set SK3 and SK4 to position ". 03 V/div.".
- Turn R6 and R7 clockwise.
- Apply a sinusoidal voltage to BU2 and BU4 of a frequency of $5 \mathrm{c} / \mathrm{s}$. Both voltages must have the same phase and the same amplitude. Both voltages must have the same phase and the same amplitude. Now an ellipse arises on the screen. In the way described in Chapter "Phase measurements", determine the angle $\varphi$ which the ellipse makes with the X axis. The deviation from $35^{\circ}$ must not exceed $5^{\circ}$.
- Repeat this measurement at frequencies of $100 \mathrm{kc} / \mathrm{s}$ and $200 \mathrm{kc} / \mathrm{s}$. Tolerance $5^{\circ}$.


## 11. Hum in the $X$ amplifier

With SK4 in position ". $03 \mathrm{~V} /$ div" the hum in the X amplifier must not exceed 0.1 division.

## 12. Crosstalk

- Set SK3 to position "0.1 V/div".
- Turn R6 and R7 clockwise.
- Set SK4 to position ". $03 \mathrm{~V} / \mathrm{div}$ ".
- Short-circuit BU4 with respect to earth.
- Apply a pulse-shaped voltage of $100 \mathrm{mV}_{\mathrm{p}-\mathrm{p}}$ to BU 2 , with a repetition frequency of $200 \mathrm{kc} / \mathrm{s}$. The X deflection must not exceed 0.2 division.


## H. TIME BASE GENERATOR

## 1. Internal triggering

- Turn R513 clockwise and R7 anti-clockwise.
- Set SK4 to position "M".
- Adjust R3 so that the time base generator has just cut out.
- Apply to BU2 a sinusoidal voltage of a frequency of $1 \mathrm{kc} / \mathrm{s}$ and an amplitude such that the picture height is 0.5 division.
- Adjust R513 in such a way that a triggered picture appears on the screen.
- Change the frequency of the input voltage successively from $5 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}$. With a correct adjustment of R3, the picture must be stationary at these frequencies, even if R7 is turned clockwise.


## 2. External triggering

- To BU7 apply a voltage of $0.5 \mathrm{~V}_{\mathrm{p}-\mathrm{p}}$ which derived from the same voltage source as the voltage applied to BU2.
- With a correct adjustment of R3, the time base generator must start smoothly and the picture must be stationary at frequencies of $5 \mathrm{c} / \mathrm{s}$ and $200 \mathrm{kc} / \mathrm{s}$.


## 3. Linearity of the time base

- Set SK2 to position ". $02 \mathrm{~ms} /$ div.".
- Apply a sinusoidal voltage to BU2, with a frequency of $50 \mathrm{kc} / \mathrm{s}$ and with such an amplitude that the picture height amounts to 8 divisions.
- Display a number of periods on the screen and by means of R7 adjust the second period from the left to a width of 2 divisions. The second period from the right may be max. 0.5 divisions wider or narrower than 2 divisions.


## 4. Time base sweep times

Set SK2 to position ". 02 ms/div.".

- Apply a square wave voltage to BU2, with a frequency such that a complete period is traced on each division of the graticule. The picture height must be 8 divisions.
- Now the value of the frequency of the square wave voltage must lie between 37.5 and $62.5 \mathrm{kc} / \mathrm{s}$. If required, correct the sweep time by selecting another value for R533.
- Check all positions of SK2 (sce table below).

| Position SK2 | Frequency square wave voltage |
| :--- | :---: |
| $.05 \mathrm{~ms} / \mathrm{div}$. | $15,000-25,000 \mathrm{c} / \mathrm{s}$ |
| $1 \mathrm{~ms} / \mathrm{div}$. | $7,500-12,500 \mathrm{c} / \mathrm{s}$ |
| $.2 \mathrm{~ms} / \mathrm{div}$. | $3,750-6,250 \mathrm{c} / \mathrm{s}$ |
| $.5 \mathrm{~ms} / \mathrm{div}$. | $1,500-2,500 \mathrm{c} / \mathrm{s}$ |
| $1 \mathrm{~ms} / \mathrm{div}$. | $750-1,250 \mathrm{c} / \mathrm{s}$ |
| $2 \mathrm{~ms} / \mathrm{div}$. | $375-625 \mathrm{c} / \mathrm{s}$ |
| $5 \mathrm{~ms} /$ div. | $150-250 \mathrm{c} / \mathrm{s}$ |
| $10 \mathrm{~ms} / \mathrm{div}$. | $75-125 \mathrm{c} / \mathrm{s}$ |
| $20 \mathrm{~ms} /$ div. | $37.5-62.5 \mathrm{c} / \mathrm{s}$ |
| $50 \mathrm{~ms} / \mathrm{div}$. | $15-25 \mathrm{c} / \mathrm{s}$ |

## Replacing parts

A. THERMAL FUSE

The supply transformer is protected by a thermal fuse which blows if the temperature of the supply transformer exceeds $125^{\circ}$. Before replacing the blown fuse, the cause must be traced first. The new fuse must be fixed to the spring " S " and then be pulled onto the hook " H " (see Fig. 20; to this end remove the rear panel and the left-hand side panel in accordance with the instructions given in section II.A).

## B. SUPPLY TRANSFORMER

- Remove the cabinet panels in accordance with the instructions given in section II.A.
- Remove the seven screws " $A$ " (see Fig. 16). Now the rear mounting plate can be pulled a little from the frame.
- Unsolder all connections of the transformer.
- Remove the four bolts and nuts"B" (Fig. 21).
- Now the transformer can be removed from the apparatus at the lefthand side.


## C. SWITCHES SK2, SK3, AND SK4

- Remove the front panel according to section II.C.
- Loosen the two screws by means of which the switch is fitted to the foremost mounting plate.


Fig. 20. Replacing the thermal fuse


Fig. 21. Replacing the supply transformer

- Unsolder the connecting wires of the switch.
- Remove the switch from the foremost mounting plate.


## D. SWITCH WAFERS SK2

- Remove the cabinet panels according to section II.A.
-- Remove the four fixing screws from the two metal mounting strips.
- Unsolder the connections of the wafer to be replaced and slide it from the switch.


## E. SWITCH WAFERS SK3

-- Remove switch SK3 according to section VI.C.

- Remove the six fixing screws from the two metal mounting strips.
- Remove the mounting strips and the trimmer holder.

Now the switch wafers can be easily removed.

## F. SWITCH WAFERS SK4

- Remove switch SK4 according to section VI.C.
- Remove the six fixing screws from the two metal mounting strips.
- Remove the mounting strips and the trimmer holder.
- Remove potentiometer R7 together with its fixing bracket.

Now the switch wafers can be easily removed.

## G. POTENTIOMETERS ON THE FRONT PANEL

- Remove the front panel according to section II.C.
- Unsolder the connections from the appropriate potentiometer.
- Remove the fixing nut from the potentiometer.
- Remove the potentiometer from the foremost mounting plate.


## H. CRT AND VALVES

## 1. Cathode ray tube

- Remove the cabinet panels according to section II.A.
- Remove the window together with the graticule according to section II.D.
- Remove anode connection "A" (Fig. 22) at the top of the cathode ray tube.


Fig. 22. Anode connection


Fig. 23. Postioning the a.r.t

- Remose the tube holder (for connection see page 877 .
- Hold the tube at the front and then pull it from the protective housing and rubber cap. When the tube is imerted it is recommended to prinkle at little talcum powder oser the lower pate of the tube so that at slide more casly into the rubher cap. See to it hat the protective cianng is mot damaged (dents etc.).
 lime base line tums exactly hormontally. It ibs is not the case. He thbe can be correctly positioned by means of lexer "H. 1 Fig. 23: \|f necesars. first loosen the screws " $k$ " it little).
Subsequently the quality of the pecture the detectorn semsitanty and the sweep time of the time base must be checked and acadusted. If neces waty (sections V.B, V.C, V.D.2. V.E. 2 and V.F.4.


## 2. Valves, diodes and other components

All component parts have heen taken from normal production stoch. After replacement of valves or other component parts it may be necessary to readjust the appropriate part of the circuit. (See chapter V, "Checking and adjusting").
New valves can be aged by allowing the apparatus to be switched on for 100 hours. Aging can also take place outside the apparatus. The valves are then connected as diodes (in the case of pentodes connect the grids and in the case of triodes the grid to the anode). The anode voltage is so chosen that the quiescent current at normal heater boltage is $1 / 6$ th of the mavimum permissible cathode current.


Fig. 24. Right-hand side view adjusting elements and units


Fig. 25. Left-hand side view with adjusting elements and units


Fig. 26. Front view with adjusting elements

The quiescent current for the various valves is as follows:
B1, B2, B501, B502, B503, B701, B702: ECF 804 mA (triode and pentode in parallel)

B3, B703
ECC 853 mA (both triodes in parallel)

B1003
$5642 \quad 0.5 \mathrm{~mA}$
ECL 827 mA (triode and pentode in parallel)

## Fault finding

The arrangement of the component parts is shown in Figs. $28 \ldots 38$. To enable faults to be traced quickly, the principal voltages and waveforms are shown in the drawings of the printed wiring boards and in the circuit diagrams. To enable faults to be remedied quickly, one should be familiar with the working of the apparatus and the instructions relating to its adjustment (chapters I and V). If necessary, you can always apply to the PHILIPS Service Organisation.
si-53 blanko

List of parts

## A. LIST OF MECHANICAL PARTS

| Item | Num-Code number ber |  | Description | Minimum slock |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Number of apparatus |  |  |  |  |
|  |  |  |  | S | 1 | 3 | 5 | 10 |
| 1 | 1 | M7 07617 | Handle | ** | - | - | - | 1 |
| 2 | 2 | E2 74267 | Bracket | ** | - | - | - | 2 |
| 3 | 1 | M7 19301 | Text plate | ** | - | - | - | 2 |
| 4 | 7 | M7773 53 | Knob $14 \mathrm{~mm} ø$ for spindle 6 mm ø | * | - | 1 | 2 | 3 |
| 5 | 5 | B1 89149 | Knob with arrow for spindle 14 mm ø | ** | - | 1 | 2 | 3 |
| 6 | 3 | 973/52 | Knob 22 mm ø | * | - | - | 1 | 2 |
| 7 | 1 | 973/D51 | Cap for knob 22 mm ø | ** | - | - | - | 1 |
| 8 | 3 | 973/P55 | Arrow for knob $22 \mathrm{~mm} \varnothing$ | ** | - | - | 1 | 2 |
| 9 | 1 | M7 35027 | Window | * | - | - | - | 2 |
| 10 | 1 | M7 74907 | Graticule | * | - | - | - | 1 |
| 11 | 1 | M7 13486 | Contrast-enhancing plate | ** | - | - | - | 1 |
| 12 | 4 | P7 65514 | Foot | ** | - | - | 2 | 4 |
| 13 | 2 | 973/58 | Knob 14 mm ø for spindle 4 mm ø | * | - | -- | 1 | 2 |
| 14 | 4 | 979/11 | Socket | * | - | 1 | 1 | 1 |
| 15 | 4 | M7 08086 | Nut | ** | - |  | 1 | 2 |
| 16 | 1 | M7 73711 | Mains voltage adapter | * | - | - | - | 1 |
| 17 | 1 | 0829050 | Mains connection | * | - | - | - | 1 |
| 18 | 2 | M760389 | Earth terminal | * | 1 | 1 | 3 | 5 |
| 19 | 1 | M7 75178 | Switch socket | * | 2 | 1 | 2 | 3 |
| 20 | 1 | P4 65588 | Box | ** | - | - | 2 | 4 |
| 21 | 1 | M7 28949 | Anode contact cap | * | - | - | 1 | 2 |
| 22 | 1 | 40467 | Valve holder (B 301) | * | - | - | - | 2 |
| 23 | 8 | $976 /$ PW $9 \times 12$ | Valve holder noval | * | 1 | 3 | 5 | 8 |
| 24 | 1 | $976 /$ PW $7 \times 12$ | Valve holder min. |  | - | - | 1 | 2 |
| 25 | 4 | $910 / 18 \times 110$ | Strip 110 mm | ** | - | - | - | 2 |


| Number | Code number | Description | Minimum stock |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Number of apparatus |  |  |  |  |
|  |  |  | S | 1 | 3 | 5 | 10 |
| 100 | A3 32036 | Soldering eyelet | ** | 10 | 10 | 15 | 25 |
| 2 | $978 / 4 \times 65$ | Coaxial plug | * | 1 | 1 | 2 | 2 |
| 2 | M7 34018 | Plug pin | * | - | 1 | 1 | 2 |
| 2 | 978/1 $\times 4 \mathrm{AP}$ | Plug | * | 1 | 2 | 2 | 3 |
| 1 m | R $209 \mathrm{KA} / 11 \mathrm{BBO}$ | H.F. cable |  | 2 | 2 | 3 | 4 |
| 2 | P5 657 09/159 AA | Trimmer holder | * | - | - | 1 | 2 |
| 10 cc | 971/71 | Switch oil | * | - | - | - | 10 cc |
| 1 | 0829049 | Female plug | * | - | - | 1 | 3 |

## Purpose of the column S

Components not marked
These should be present at the Service Department in the country concerned or at the customer's who is using the apparatus.
They include:
a. nearly all electrical components;
b. mechanical parts which are vulnerable, or which are subject to wear.

## Components marked with one star

These components generally have a long or unlimited service-life, but their presence is essential for the correct working of the apparatus. Stocking up of a few of these components depends on the following factors.
a. the number of apparatus present in the country concerned;
b. the necessity of having the apparatus working continuously or not;
c. the time of delivery of the components with respect to the import restrictions in the country concerned and the duration of the transport.

## Components marked with two stars

These components have a long or unlimited service-life and they are not essential for the correct working of the apparatus. Generally there is not a local stock.


## B. LIST OF ELECTRICAL PARTS ELEKTRISCHE EINZELTEILE

## ELEKTRISCHE ONDERDELEN NOMENCLATURE ELECTRIQUE

- The indication "PW" means, that the component concerned is a of type for mounting on a printed-wiring plate.
- Die Angabe „PW" bedeutet, dass der diesbezügliche Teil speziell für Montage auf Leiterplatten bestimmt ist.
- De aanduiding „PW" betekent, dat het desbetreffende onderdeel speciaal voor montage op gedrukte bedradingsplaten is bestemd.
- L'indication "PW" indique, que cette pièce est du type pour montage sur une plaque de câblage imprimé.
- The correct values of selected resistors and capacitors have been fixed when adjusting the instrument in the factory.
- Die richtigen Werte der Abgleichwiderständen und -Kapazitäten sind bei der Einstellung in der Fabrik festgelegt.
- De juiste waarden van de keuzeweerstanden en -condensatoren zijn bij het afregelen in de fabriek bepaald.
- Les valeurs exactes des résistances et des capacités d'ajustage sont choisies lors de la fabrication de l'appareil.
- All resistors are vaporized carbon resistors, unless otherwise stated.
- Sofern nicht anders angegeben, handelt es sich hierbei um Kohlewiderstände.
- Alle weerstanden zijn opgedampte koolweerstanden, tenzij anders aangegeven.
- Toutes les résistances sont du type au carbone vaporisé, sauf indication différente.

Für die englische Wörter lese man in deutsch, holländisch oder französisch:
Voor de Engelse tekst kan men in het Duits, Nederlands of Frans lezen: Pour le texte anglais on lit en allemand, hollandais ou en français:

| Service part | Bestellnummer | Bestelnummer | Numéro de code |
| :--- | :--- | :--- | :--- |
| Value | Wert | Waarde | Valeur |
| Tolerance | Fehlergrenzen | Tolerantie | Tolérance |
| Power | Leistung | Vermogen | Wattage |
| Voltage | Spannung | Spanning | Tension |
| Description | Beschreibung | Omschrijving | Désignation |
| Potentiometer <br> (potm) linear | Pot. linear | Lincaire koolpot. | Potentiométre au <br> carbon linéair <br> Wire-wound |
| Drahtwiderstand |  | Draadgewonden | Bobineé |
| 2 in parallel | 2 parallel | 2 parallel | 2 en parallèle |
| Choice resistor | Abgleichwiderstand | Keuzeweerstand | Résistance d'ajustage |

Capacitors-Kondensatoren-Condensatoren-Condensateurs

| No. | Service part | Value | Voliage <br> $V$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| C26 | $906 / \mathrm{V} 100 \mathrm{~K}$ | $0.1 \mathrm{\mu F}$ | 700 | 10 | Paper |
| C27 | C 004 FA/20E | 20 pF |  |  | Trimmer |
| C28 | $908 / \mathrm{P} 10 \mathrm{E}$ | 10 pF |  |  | Trimmer |
| C29 | C $004 \mathrm{FA} / 20 \mathrm{E}$ | 20 pF |  |  | Trimmer |
| C30 | $904 / 22 \mathrm{E}$ | 22 pF | 500 | 10 | Ceramic |
| C31 | $904 / 1 \mathrm{~K}$ | 1000 pF | 500 | $-20 /+50$ | Ceramic |
| C32 | $904 / 10 \mathrm{E}$ | 10 pF | 500 | $\pm 3 \mathrm{pF}$ | Ceramic |
| C33 | $904 / 56 \mathrm{E}$ | 56 pF | 500 | 10 | Ceramic |
| C34 | $906 / 22 \mathrm{~K}$ | 22000 pF | 400 | 10 | Polyester |
| C35 | $904 / 2 \mathrm{~K} 2$ | 2200 pF | 500 | $-20 /+50$ | Ceramic |
| C36 | $904 / 270 \mathrm{E}$ | 270 pF | 500 | 10 | Ceramic |
| C37 | $904 / 270 \mathrm{E}$ | 270 pF | 500 | 10 | Ceramic |
| C38 | $904 / 680 \mathrm{E}$ | 680 pF | 500 | $-20 /+50$ | Ceramic |
| C39 | $904 / 8 \mathrm{E} 2$ | 8.2 pF | 500 | $\pm \frac{1}{2} \mathrm{pF}$ | Ceramic |

Resistors-Widerstände-Weerstanden-Résistances

| No. | Service part | Value | Power <br> $W$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R4 | E 091 CG/00B12 | $500 \mathrm{k} \Omega$ |  |  | Potm. tandem lin. |
| R6 | $916 / \mathrm{GL} 200 \mathrm{~K}$ | $200 \mathrm{k} \Omega$ |  |  | Potm. log. |
| R25 | $901 / 1 \mathrm{M}$ | $1 \mathrm{M} \Omega$ | 0.25 | 1 | 1 |
| R26 | $901 / 200 \mathrm{~K}$ | $0.2 \mathrm{M} \Omega$ | 0.25 | 1 |  |
| R27 | B8 305 23D/52K6 | $52600 \Omega$ | 0.25 | 1 |  |
| R28 | $901 / 12 \mathrm{~K}$ | $12 \mathrm{k} \Omega$ | 0.1 | 1 |  |
| R29 | B8 305 25D/3K33 | $3330 \Omega$ | 1 | 1 |  |
| R30 | B8 305 25D/1K16 | $1160 \Omega$ | 0.1 | 1 |  |
| R31 | B8 305 25D/333E | $333 \Omega$ | 0.1 | 1 |  |
| R32 | B8 305 25D/167E | $167 \Omega$ | 0.1 | 1 |  |
| R34 | B8 305 26D/333K | $333 \mathrm{k} \Omega$ | 0.25 | 1 |  |
| R35 | B8 305 17D/450K | $450 \mathrm{k} \Omega$ | 0.25 | 1 |  |
| R36 | B8 305 26D $/ 483 \mathrm{~K}$ | $483 \mathrm{k} \Omega$ | 0.25 | 1 |  |

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| No. | Service part | Value | Power <br> W | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R37 | $901 / 100 \mathrm{~K}$ | $0.1 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R38 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R40 | $4876605 / 22 \mathrm{~K}$ | $22 \mathrm{k} \Omega$ | 8 | 5 | Wire-wound |
| R41 | $901 / 1 \mathrm{M}$ | $1 \mathrm{M} \Omega$ | 0.25 | 5 |  |
| R42 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R43 | $901 / 4 \mathrm{~K} 7$ | $4700 \Omega$ | 0.25 | 5 |  |
| R44 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R45 | $938 / \mathrm{B} 20 \mathrm{~K}$ | $20 \mathrm{k} \Omega$ | 8 | 5 |  |
| R47 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 | Wire-wound |
| R48 | $901 / 12 \mathrm{~K}$ | $12 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R49 | $901 / 4 \mathrm{~K} 7$ | $4800 \Omega$ | 0.25 | 5 |  |
| R55 | $901 / 3 \mathrm{~K} 3$ | $3300 \Omega$ | 0.25 | 5 |  |
| R56 | $901 / 12 \mathrm{~K}$ | $12 \mathrm{k} \Omega$ | 0.25 | 1 |  |
| R57 | $916 / \mathrm{GE} 500 \mathrm{~K}$ | $500 \mathrm{k} \Omega$ |  |  |  |
| R58 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R59 | $901 / 1 \mathrm{~K} 5$ | $1500 \Omega$ | 0.25 | 5 |  |
| R62 | $901 / 1 \mathrm{~K} 5$ | $1500 \Omega$ | 0.25 | 5 |  |
| R63 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R64 | $901 / 100 \mathrm{~K}$ | $0.1 \mathrm{M} \Omega$ | 0.25 | 5 |  |
| R67 | $901 / 82 \mathrm{~K}$ | $82 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R68 | $901 / 82 \mathrm{~K}$ | $82 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R70 | $901 / 100 \mathrm{~K}$ | $0.1 \mathrm{M} \Omega$ | 0.25 | 5 |  |
| R71 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R72 | $901 / 6 \mathrm{M} 8$ | $6.8 \mathrm{M} \Omega$ | 0.25 | 10 |  |
| R73 | $901 / 27 \mathrm{~K}$ | $27 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R76 | $901 / 6 \mathrm{M} 8$ | $6.8 \mathrm{M} \Omega$ | 0.25 | 10 |  |
| R77 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R79 | $901 / 27 \mathrm{~K}$ | $27 \mathrm{k} \Omega$ | 0.5 | 5 |  |
| R70 | $\mathrm{E} 098 \mathrm{CG} / 00 \mathrm{~A} 01$ | $1 \mathrm{k} \Omega$ |  |  |  |
| R81 | $901 / 8 \mathrm{~K} 2$ | $8200 \Omega$ | 0.5 | 5 |  |
| R82 | $901 / 15 \mathrm{~K}$ | $15 \mathrm{k} \Omega$ | 0.5 | 5 |  |
| R85 | $901 / 6 \mathrm{~K} 8$ | $6800 \Omega$ | 0.5 | 5 |  |

Valves-Röhren-Buizen-Tubes
B1 ECF 80
B2 ECF 80
B3 ECC 85


Fig. 28. Unit A; Y-amplifier


Fig. 29. Diagram of the Y-amplifier
$60+69$ blamko



B501-502-503
$R 522=47 \mathrm{k} \Omega$
RS20 is connected in parallel with R 522
Fig. 31. Diagram of the trigger-pulse shaper and of the time-base generator

Capacitors-Kondensatoren-Condensatoren-Condensateurs

| No. | Service part | Value | Voltage <br> $V$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |  |  |
| C501 | $904 / 22 \mathrm{~K}$ | 22000 pF | 500 | $-20 /+50$ | Ceramic |
| C502 | $904 / 27 \mathrm{E}$ | 27 pF | 500 | 10 | Ceramic |
| C503 | $904 / 27 \mathrm{E}$ | 27 pF | 500 | 10 | Ceramic |
| C504 | $904 / 15 \mathrm{E}$ | 15 pF | 500 | 10 | Ceramic |
| C505 | $906 / 470 \mathrm{~K}$ | $0.47 \mu \mathrm{~F}$ | 400 | 10 | Polyester |
| C506 | $906 / 220 \mathrm{~K}$ | $0.22 \mu \mathrm{~F}$ | 400 | 10 | Polyester |
| C507 | $906 / 100 \mathrm{~K}$ | $0.1 \mu \mathrm{~F}$ | 400 | 10 | Polyester |
| C508 | $906 / 47 \mathrm{~K}$ | 47000 pF | 400 | 10 | Polyester |
| C509 | $906 / 22 \mathrm{~K}$ | 22000 pF | 400 | 10 | Polyester |
| C510 | $906 / 10 \mathrm{~K}$ | 10000 pF | 400 | 10 | Polyester |
| C511 | $906 / 4 \mathrm{~K} 7$ | 7400 pF | 400 | 10 | Polyester |
| C512 | $906 / 2 \mathrm{~K} 2$ | 2200 pF | 400 | 10 | Polyester |
| C513 | $904 / 820 \mathrm{E}$ | 820 pF | 500 | $-20 /+50$ | Ceramic |
| C514 | $904 / 390 \mathrm{E}$ | 390 pF | 500 | 10 | Ceramic |
| C515 | $904 / 180 \mathrm{E}$ | 180 pF | 500 | 10 | Ceramic |
| C516 | $904 / 68 \mathrm{E}$ | 68 pF | 500 | 10 | Ceramic |
| C517 | $904 / 120 \mathrm{E}$ | 120 pF | 500 | 10 | Ceramic |
| C518 | AC 8128/8 | $8 \mu \mathrm{~F}$ | 350 |  | Electrolytic (PW) |
| C519 | $906 / \mathrm{V} 82 \mathrm{~K}$ | 82000 pF | 700 | 10 | Paper |

Resistors-Widerstände-Weerstanden-Résistances

| No. | Service part | Value | Power <br> $W$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R3 | $916 / \mathrm{GE} 20 \mathrm{~K}$ | $20 \mathrm{k} \Omega$ |  |  | Potm. lin. |
| R501 | $901 / 120 \mathrm{~K}$ | $120 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R502 | $901 / 1 \mathrm{M}$ | $1 \mathrm{M} \Omega$ | 0.25 | 5 |  |
| R503 | $901 / 220 \mathrm{~K}$ | $220 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R504 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R505 | $901 / 1 \mathrm{~K}$ | $1 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R506 | $901 / 82 \mathrm{~K}$ | $82 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R507 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R508 | $901 / 22 \mathrm{~K}$ | $22 \mathrm{k} \Omega$ | 0.25 | 5 |  |


| $N o$. | Service part | Value | Power W | Tolerance \% | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R509 | 901/4K7 | $4700 \Omega$ | 0.5 | 5 |  |
| R510 | 901/150K | $150 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R511 | E $003 \mathrm{AG} / \mathrm{D} 47 \mathrm{~K}$ | $47 \mathrm{k} \Omega$ | 1 | 1 |  |
| R512 | 901/68K | $68 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R513 | E098 CG/00A08 | $100 \mathrm{k} \Omega$ |  |  | Potm. lin |
| R514 | 901/120K | $120 \mathrm{k} \Omega$ | 0.5 | 5 | Potm. |
| R516 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R517 | 901/1K5 | $1500 \Omega$ | 0.25 | 5 |  |
| R518 | 901/3K3 | $3300 \Omega$ | 0.5 | 5 |  |
| R519 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R520 | 901/100K-4M7 | 0.1-4.7 | 2 |  | par. with R 522 |
| R521 | 48766 05/18K | $18 \mathrm{k} \Omega$ | 8 | 5 | Wire-wound |
| R522 | 902/K47K | $47 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R523 | 901/82K | $82 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R524 | 901/82K | $82 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R525 | E 003 AG/D68K | $68 \mathrm{k} \Omega$ | 1 | 5 |  |
| R527 | E 003 AG/D33K | $33 \mathrm{k} \Omega$ | 1 | 5 |  |
| R528 | 48766 05/22K | $22 \mathrm{k} \Omega$ | 8 | 5 | Wire-wound |
| R529 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 | Wire-wound |
| R530 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R531 | 901/10M | $10 \mathrm{M} \Omega$ | 0.5 | 10 |  |
| R532 | E003 AG/D47K | $47 \mathrm{k} \Omega$ | 1 | 1 |  |
| R533 | 901/ |  | 0.25 | 5 | Choice resistor |

## Valves-Röhren-Buizen-Tubes-Diodes

B501 ECF 80
B502 ECF 80
B503 ECF 80
GR503 0A202

Capacitors-Kondensatoren-Condensatoren-Condensateurs

| No. | Servicepart | Value | Voliage <br> $V$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| C726 | $906 / \mathrm{V} 100 \mathrm{~K}$ | $0.1 \mu \mathrm{~F}$ | 700 | 10 | Paper |
| C727 | C 004 FA/20E | 20 pF |  |  | Trimmer |
| C728 | $908 / \mathrm{P} 10 \mathrm{E}$ | 10 pF |  |  | Trimmer |
| C729 | C 004 FA/20E | 20 pF |  |  | Trimmer |
| C730 | $904 / 22 \mathrm{E}$ | 22 pF | 500 | 10 | Ceramic |
| C731 | $904 / 1 \mathrm{~K}$ | 1000 pF | 500 | $-20 /+50$ | Ceramic |
| C732 | $904 / 10 \mathrm{E}$ | 10 pF | 500 | $\pm 0.5 \mathrm{pF}$ | Ceramic |
| C733 | $904 / 56 \mathrm{E}$ | 56 pF | 500 | 10 | Ceramic |
| C734 | $906 / 22 \mathrm{~K}$ | 22000 pF | 400 | 10 | Polyester |
| C735 | $904 / 2 \mathrm{~K} 2$ | 2200 pF | 500 | $-20 /+50$ | Ceramic |
| C736 | $904 / 150 \mathrm{E}$ | 150 pF | 500 | 10 | Ceramic |
| C737 | $904 / 150 \mathrm{E}$ | 150 pF | 500 | 10 | Ceramic |
| C738 | $904 / 560 \mathrm{E}$ | 560 pF | 500 | 10 | Ceramic |
| C739 | $906 / \mathrm{L} 100 \mathrm{~K}$ | $0.1 \mu \mathrm{~F}$ | 125 | 10 | Polyester |

Resistors-Widerstände-Weerstanden-Résistances

| No. | Servicepart | Value | Power <br> $W$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R5 | E 091 CG/00B12 | $500 \mathrm{k} \Omega$ |  |  | Potm.tandem lin. |
| R7 | 916/GL 200K | $200 \mathrm{k} \Omega$ |  |  | Potm. log. |
| R725 | $901 / 1 \mathrm{M}$ | $1 \mathrm{M} \Omega$ | 0.25 | 1 |  |
| R726 | B8 305 26D/176K | $176 \mathrm{k} \Omega$ | 0.25 | 1 |  |
| R727 | B8 305 23D/52K6 | $52600 \Omega$ | 0.25 | 1 |  |
| R728 | B8 305 23D/20K4 | $10200 \Omega$ | 0.1 | 1 | (2 in par.) |
| R729 | B8 305 25D/3K53 | $3530 \Omega$ | 0.1 | 1 |  |
| R730 | $901 / 1 \mathrm{~K}$ | $1 \mathrm{k} \Omega$ | 0.1 | 1 |  |
| R731 | B8 305 23D/500E | $500 \Omega$ | 0.1 | 1 |  |
| R732 | $901 / 27 \mathrm{~K}-150 \mathrm{~K}$ | $27-150 \mathrm{k} \Omega$ |  |  | par. with R733 |
| R733 | $902 / \mathrm{K} 2 \mathrm{~K} 7$ | $2.7 \mathrm{k} \Omega$ | 0.25 | 5 | Choice resistor |
| R734 | B8 305 26D/350K | $350 \mathrm{k} \Omega$ | 0.25 | 1 |  |
| R735 | B8 305 17D/450K | $450 \mathrm{k} \Omega$ | 0.25 | 1 |  |
| R736 | B8 305 26D/485K | $485 \mathrm{k} \Omega$ | 0.25 | 1 |  |


| $N o$. | Service part | Value | Power W | Tolerance $\%$ | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R737 | 901/100K | $100 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R738 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R739 | 901/270K | $270 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R740 | 48766 05/22K | $22 \mathrm{k} \Omega$ | 8 | 5 | Wire-wound |
| R741 | $901 / 1 \mathrm{M}$ | $1 \mathrm{M} \Omega$ | 0.25 | 5 |  |
| R742 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R743 | 901/4K7 | $4.7 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R744 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R745 | 938/B20K | $20 \mathrm{k} \Omega$ | 8 | 5 | Wire-wound |
| R746 | E $097 \mathrm{AD} / 10 \mathrm{~K}$ | $10 \mathrm{k} \Omega$ |  |  | Potm. (PW) |
| R747 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R748 | 901/12K | $12 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R749 | 901/4K7 | $4.7 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R755 | 901/3K3 | $3.3 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R756 | 901/12K | $12 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R757 | 916/GE 500K | $500 \mathrm{k} \Omega$ |  |  | Potm. lin. |
| R758 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R759 | 901/1K5 | $1.5 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R762 | 901/1K5 | $1.5 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R763 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R764 | 901/100K | $100 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R767 | 901/82K | $82 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R768 | 901/82K | $82 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R770 | 901/100K | $100 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R771 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R772 | 901/2M2 | 2.2 M $\Omega$ | 0.25 | 10 |  |
| R773 | 901/27K | $27 \mathrm{k} \Omega$ | 0.5 | 5 |  |
| R776 | 901/2M2 | $2.2 \mathrm{M} \Omega$ | 0.25 | 10 |  |
| R777 | 901/100E | $100 \Omega$ | 0.25 | 5 |  |
| R779 | 901/27K | $27 \mathrm{k} \Omega$ | 0.4 | 5 |  |
| R780 | E 098 CG/00A01 | $1 \mathrm{k} \Omega$ |  |  | Potm. lin. |
| R781 | E 003 AG/D15K | $15 \mathrm{k} \Omega$ | 1 | 5 |  |
| R782 | E 003 AG/D15K | $15 \mathrm{k} \Omega$ | 1 | 5 |  |
| Valves-Röhren-Buizen-Tubes |  |  |  |  |  |
| B701 | ECF 80 |  |  |  |  |
| B702 | ECF 80 |  |  |  |  |
| B703 | ECC 85 |  |  |  |  |



Fig. 32. Unit $C$; X-amplifier


R732 is connected in parallel with R733
Fig. 33. Diagram of the $X$-amplifier

Capacitor-Kondensator-Condensator-Condensateur

|  |  | Value | Voltage <br> $V$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| No. | Service part |  | 10000 pF | 400 | 10 |

Resistors-Widerstānde-Weerstanden-Résistances

| No. | Service part | Value | Power <br> $W$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R2 | $916 / \mathrm{GE} 500 \mathrm{~K}$ | $500 \mathrm{k} \Omega$ |  |  | Potm. lin. |
| R301 | $901 / 10 \mathrm{M}$ | $10 \mathrm{M} \Omega$ | 0.25 | 10 |  |
| R302 | $901 / 470 \mathrm{~K}$ | $470 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R303 | $901 / 56 \mathrm{~K}$ | $56 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R304 | $901 /$ |  |  |  | Choice resistor |
| R305 | E 098 CG/00A15 | $1 \mathrm{M} \Omega$ | 0.25 | 5 | Potm. lin. |
| R307 | $901 / 220 \mathrm{~K}$ | $220 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R308 | $901 / 470 \mathrm{~K}$ | $470 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R309 | $916 / \mathrm{GE} 500 \mathrm{~K}$ | $500 \mathrm{k} \Omega$ |  |  | Potm. lin. |

Valve-Röhre-Buis--Tube-Diode

B301 DH7-78
GR301 0A 202


Fig. 34. Unit B; beam control
$-86-$


Fig. 35. Diagram of the cathode-ray tube circuit

$$
108+84 \text { blink. }
$$

Capacitors-Kondensatoren-Condensatoren-Condensateurs

| No. | Service part | Value | Voltage <br> $V$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Cl001 | $\mathrm{AC} 8311 / 12,5+12,5$ | $12.5 \mu \mathrm{~F}$ | 500 |  | Electrolytic (PW) |
| C 1002 | $\mathrm{AC} 8211 / 16$ | $16 \mu \mathrm{~F}$ | 500 |  | Electrolytic |
| C 1003 | $906 / 47 \mathrm{~K}$ | 47000 pF | 400 | 10 | Polyester |
| C 1004 | $\mathrm{AC} 8311 / 12,5+12,5$ | $12,5 \mu \mathrm{~F}$ | 500 |  | See Cl001 |
| C 1005 | $906 / 47 \mathrm{~K}$ | 47000 pF | 400 | 10 | Polyester |
| C 1006 | $903 / \mathrm{N} 200 \mathrm{~K}$ | $0.2 \mu \mathrm{~F}$ | 2000 |  | Box capacitor |
| C 1007 | $\mathrm{AC} 8210 / 16$ | $16 \mu \mathrm{~F}$ | 450 |  | Electrolytic (PW) |
| C1008 | $\mathrm{AC} 8210 / 16$ | $16 \mu \mathrm{~F}$ | 450 |  |  |

Resistors-Widerstände-Weerstanden-Résistances

| No. | Service part | Value | Power <br> $W$ | Tolerance <br> $\%$ | Description |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R1 | $916 / \mathrm{DE} 1 \mathrm{M}$ | $1 \mathrm{M} \Omega$ |  |  | Potm. lin. with <br> switch |
| R1003 | $931 / \mathrm{A} 4 \mathrm{~K} 7$ |  |  |  | Wire-wound |
| R1004 | $902 / \mathrm{K} 27 \mathrm{E}$ | $4.7 \mathrm{k} \Omega$ | 16 | 10 |  |
| R1005 | $901 / 1 \mathrm{M}$ | $27 \Omega$ | 0.25 | 5 |  |
| R1006 | $901 / 100 \mathrm{E}$ | $1 \mathrm{M} \Omega$ | 0.25 | 5 |  |
| R1007 | $901 / 100 \mathrm{E}$ | $100 \Omega$ | 0.25 | 5 |  |
| R1008 | $901 / 120 \mathrm{~K}$ | $100 \Omega$ | 0.25 | 5 |  |
| R1009 | $901 / 1 \mathrm{M} 2$ | $120 \mathrm{k} \Omega$ | 0.5 | 5 |  |
| R1010 | $901 / 4 \mathrm{M} 7$ | $1.2 \mathrm{M} \Omega$ | 0.25 | 10 |  |
| R1011 | $901 / 6 \mathrm{~K} 8-15 \mathrm{~K}$ | $4.7 \mathrm{M} \Omega$ | 0.25 | 10 |  |
| R1012 | $901 / 390 \mathrm{~K}$ | $6.8 \mathrm{k} \Omega-15 \mathrm{k} \Omega$ | 0.25 | 5 | Choice resistor |
| R1013 | $901 / 22 \mathrm{~K}$ | $390 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R1018 | $938 / \mathrm{A} 6 \mathrm{~K} 8$ | $22 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R1019 | $901 / 560 \mathrm{~K}$ | $6.8 \mathrm{k} \Omega$ | 5.5 | 5 | Wire-wound |
| R1020 | $901 / 680 \mathrm{~K}$ | $560 \mathrm{k} \Omega$ | 0.25 | 5 |  |
| R1021 | $901 / 680 \mathrm{~K}$ | $680 \mathrm{k} \Omega$ | 0.25 | 5 |  |

Other components - Übrige Teile - Overige onderdelen - D'autres pieces

| B1001 | ECL 82 |  |
| :---: | :---: | :---: |
| B1002 | 85 A2 |  |
| B1003 | 5642 |  |
| GR1001 | OA 214 |  |
| GR1002 | OA 214 |  |
| GR1003 | OA 214 |  |
| GR1004 | OA 214 |  |
| GR1005 | B 250 C 75 |  |
| VL1 | 974/T125 | Thermal fuse $125^{\circ} \mathrm{C}$ |
| T1001 | M7 61528 | Mains transformer |



PEM 305
E 114

Fig. 36. Unit E; high tension unit


Fig. 37. Unit F; supply




SKLI


PEM 301
E 130







R1021 $=680 \mathrm{k} \Omega \mathrm{VLI}$ is situated on the other side of point

Fig. 38. Diagram of the supply pa

